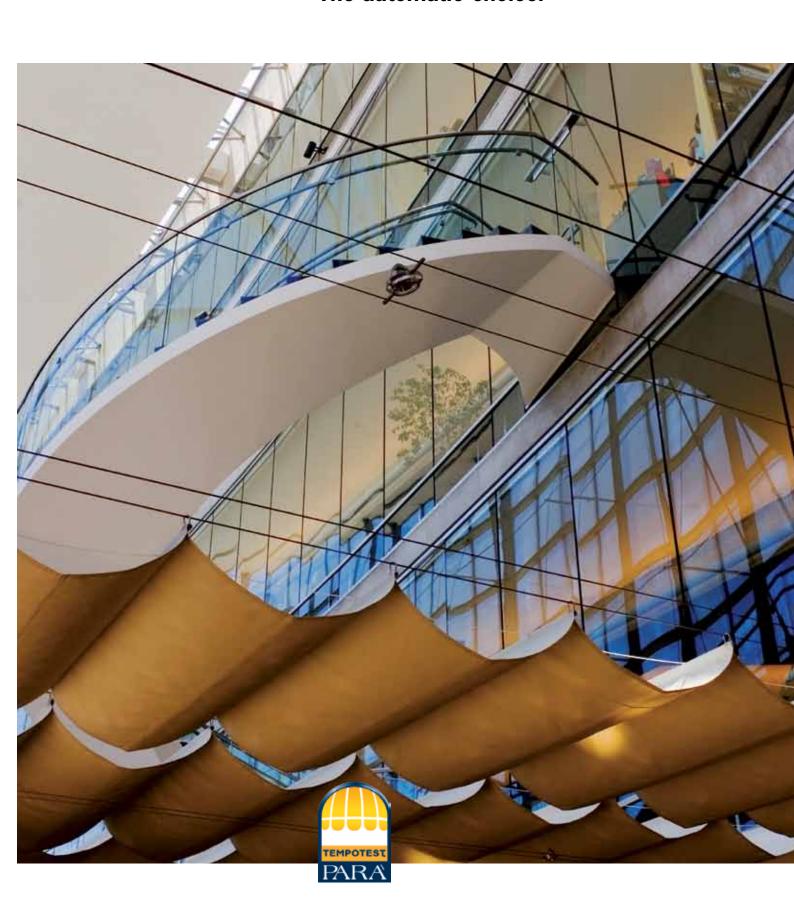
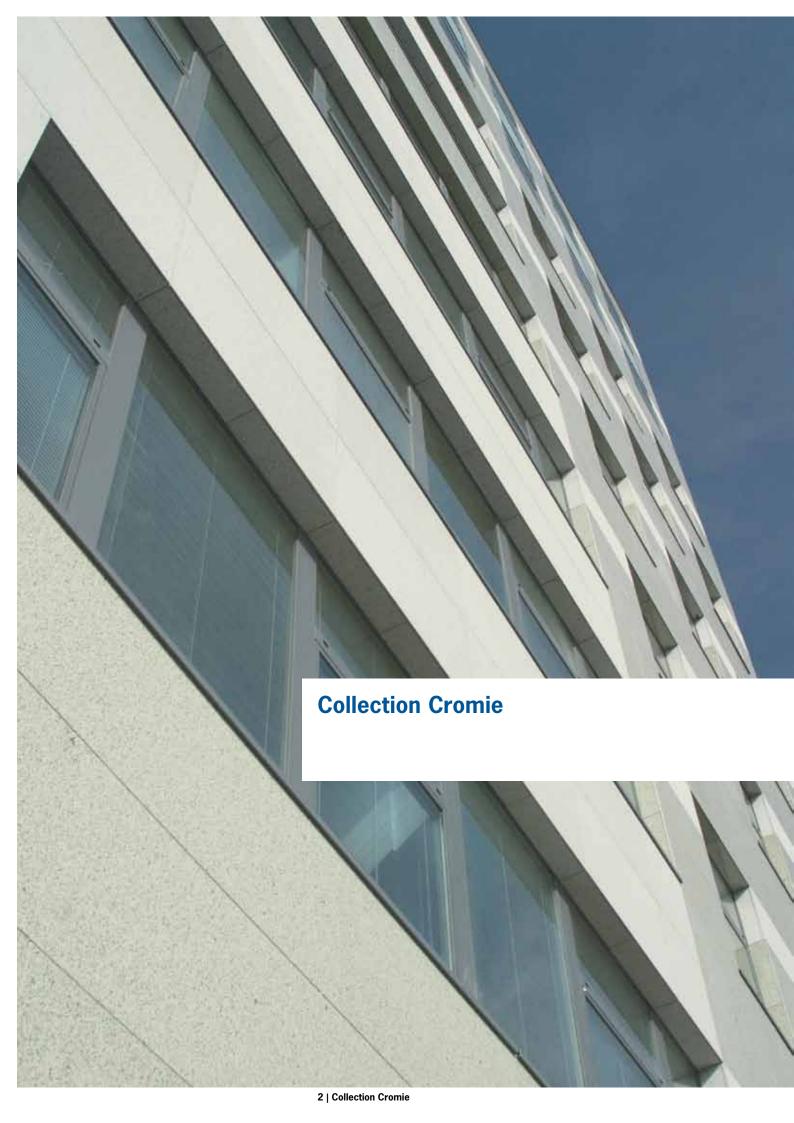


Collection Cromie. The automatic choice.





The Collection Cromie is a functional interpretation in favor of esthetics: The technical properties of acrylic fibers with mass coloration are freshened up with minimalist patterns and colors, thus allowing them to fit in with the architectural structures, facade materials and ambience of the surroundings. They withstand all climatic conditions and atmospheric influences as well as UV radiation and the most aggressive forms of environmental pollution. The Collection Cromie is available in three color schemes:



URBAN STYLE

Simple and elegant in color and form. The look of Urban Style is reminiscent of the flair of a pulsating city.



COUNTRY STYLE

Country Style reproduces the concentrated appeal of a romantic rural setting in a uniquely esthetic way.



SEA SIDE

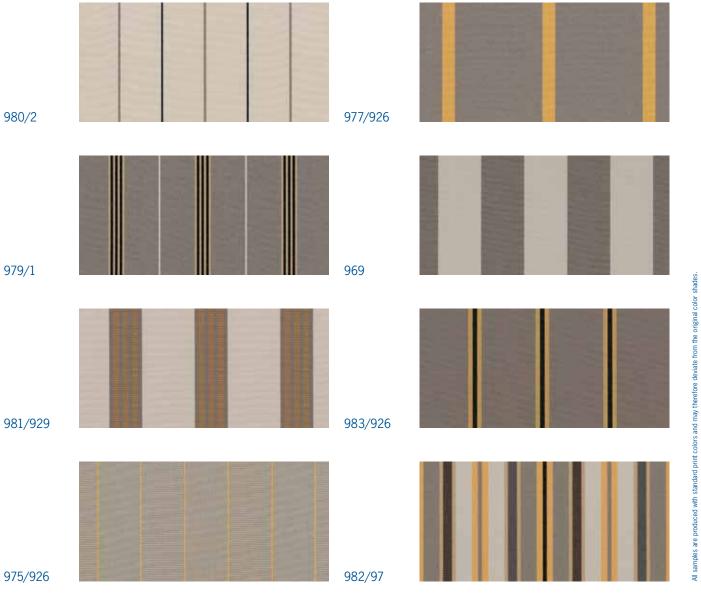
Sea Side enriches the collection with a Mediterranean touch: summery, clear colors, reminiscent of rocky cliffs, seawater and the sun.

ACRYLIC TECHNOLOGY

Griesser acrylic fabrics have been in use for generations. Having been on the market for over 40 years, they convince thanks to their extraordinary durability and long-lasting color brilliance. The color pigment is stored in each individual fiber during the creation of the basic acrylic material. The result is especially high color brilliance and great UV resistance. This dyeing of the basic material makes Griesser fabrics superior to the products of other manufacturers, in which only the finished threads are dyed. The basic acrylic material consists of many small fibers, which become entangled with each other to create a wadded source material. This basic material later ensures particularly pleasant haptic textile qualities in the woven fabric. The wad is subsequently spun: during the spinning process the individual fibers are gradually aligned to be increasingly straight until they lie close to each other and are brought together as a single thread. The advantage of Griesser acrylic fabric: Thanks to the vertical production process – from spinning, weaving and equipment to the finished fabric – product optimizations and innovations can be implemented faster.



Urban Style



4 | Collection Cromie

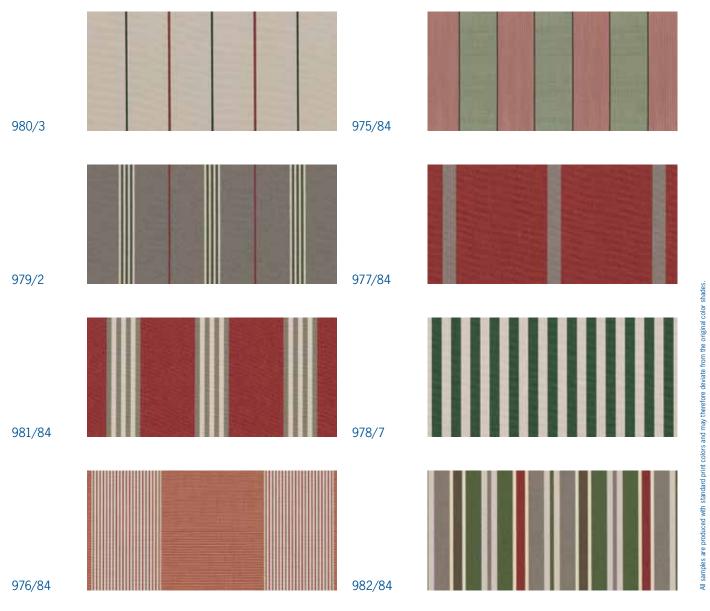




5 | Collection Cromie



Country Style



6 | Collection Cromie

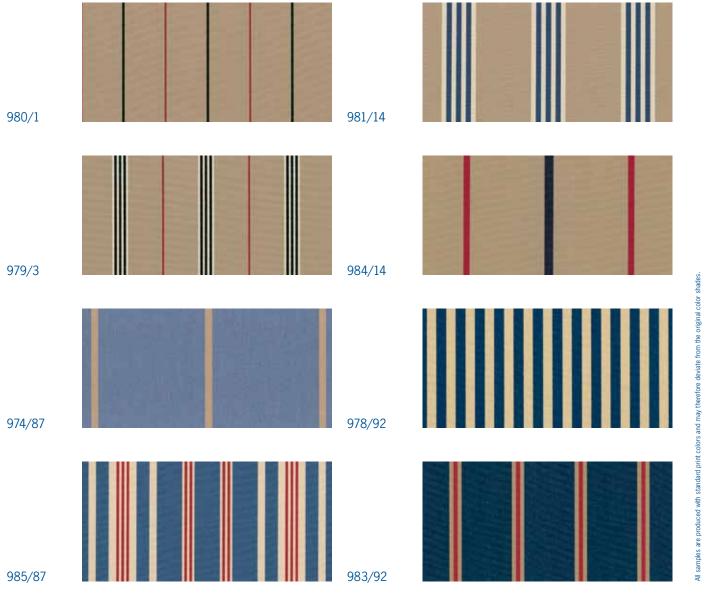




7 | Collection Cromie



Sea Side



8 | Collection Cromie





9 | Collection Cromie



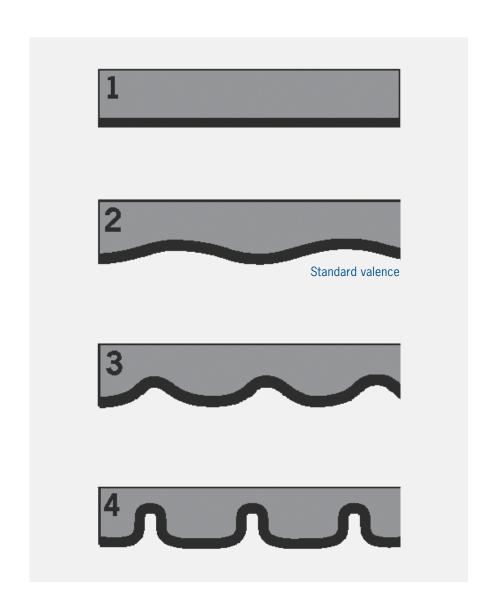
10 | Collection Cromie

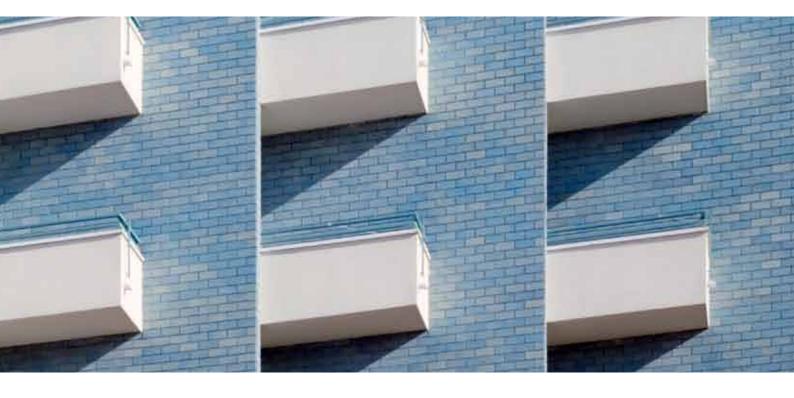


11 | Collection Cromie



Valence and valence edge bindings









Folding crease dark in transmitted light



Waviness next to a seam



Finissaggio ad alta tecnologia High technology finishing 'High-technology" Ausrüstung Acabado de alta tecnología



KEY

SPF

= transmission coefficient solar spectrum

 T_{v} = transmission coefficient visible spectrum

 R_{ρ} = reflection coefficient solar spectrum

= reflection coefficient R_v visible spectrum

HS = heat protection

LS = light protection

BS = glare protection

= sun protection factor (UV protection factor)

= total energy transmittance g-tot_e

PRODUCT CHARACTERISTICS OF AWNING FABRICS

The fabric of an awning primarily offers protection from glares, UV radiation and excessive heat. In addition, the forms and colors of the fabric pattern convey a pleasant atmosphere. Despite modern and meticulous production processes, it is not possible to avoid minor blemishes in processed fabrics. For this reason, we unfortunately have to rule these out as a grounds for complaint. The technical fabrics we process meet strict technical requirements and are subjected to comprehensive laboratory tests in the production process. The most widely varying characteristics are consistently checked using recognized measurement processes.

CREASES

Creases arise during the production and folding of the sun protection fabric. A dark line can be seen at the crease location against the light, especially in the case of light

WAVINESS IN THE SEAM AREA

Awning fabrics are normally produced from strips about 120 cm wide. When sewn together, an upper and lower layer of fabric arises in the seam and hem area. If the awning fabric is rolled up, tension arises between these layers of fabric, since the upper fabric strip has to cover a longer distance than the lower during rolling. The seams and side hem are overstretched across the entire rolling length of the fabric. This leads to sagging in this area - the fabric becomes wavy here. This unavoidable effect has no influence on the quality, function or durability of the fabrics.

HONEYCOMBING EFFECT

Awning fabrics are sewn in the projection direction to enable the tensile stress to act on the warp threads. These are woven more densely than the weft threads for optimal absorption of the tensile forces. This creates the honeycombing effect, depending on weather conditions and fabric sizes. This effect is reinforced by unfavorable light or moisture - especially if the fabric is retracted while wet. To enable rainwater to flow off, the fabric slant must be at least 14°. This counteracts the formation of water deposits and dirt streaks. The honeycombing can extend up to the center of the fabric strip. This effect has no influence on the quality, function or durability of the fabrics.

DIRT-, WATER- AND OIL-REPELLENT

Thanks to the innovative nano-coating on Griesser fabrics, dirt simply rolls right off.

SAFE FOR PEOPLE AND THE ENVIRONMENT

The Oeko-Text Standard 100 quality seal guarantees that Griesser fabrics do not contain any materials that could be harmful to health or the environment.

980/2	MATERIAL NO.	T _e	T _v	R_{e}	R _v	HS	LS	BS	SPF	g-tot _e
979/1 0.10 0.08 0.35 0.34 90 92 T, <10% 80 0.12 975/926 0.17 0.14 0.50 0.48 83 86 > 10.05, T, <20% 40 0.15 975/926 0.19 0.16 0.52 0.49 81 84 > 10%, T, <20% 40 0.15 975/926 0.11 0.09 0.42 0.39 89 91 T, <10% 80 0.12 983/926 0.09 0.07 0.38 0.35 91 93 T, <10% 80 0.12 983/926 0.09 0.07 0.38 0.35 91 93 T, <10% 80 0.12 983/926 0.09 0.07 0.38 0.35 91 0.05 T, <10% 80 0.13 983/926 0.09 0.07 0.38 0.35 91 0.05 T, <10% 80 0.13 983/926 0.09 0.07 0.38 0.35 91 0.05 T, <10% 80 0.15 983/926 0.09 0.07 0.38 0.35 91 0.05 T, <10% 80 0.15 983/926 0.09 0.07 0.38 0.35 91 0.05 T, <10% 80 0.15 983/926 0.09 0.07 0.38 0.35 91 0.05 T, <10% 80 0.15 983/926 0.09 0.07 0.38 0.35 91 0.05 T, <10% 80 0.15 983/926 0.09 0.07 0.04 0.39 0.34 0.39 87 90 > 10%, T, <20% 40 0.15 983/926 0.18 0.17 0.52 0.49 82 83 > 10%, T, <20% 40 0.15 985/15 0.17 0.13 0.43 0.40 83 87 > 10%, T, <20% 40 0.15 926 0.07 0.04 0.39 0.34 0.39 9.3 96 T, <10% 80 0.11 926 0.07 0.04 0.39 0.34 0.39 9.3 96 T, <10% 80 0.11 930 0.04 0.10 0.25 0.10 96 99 T, <10% 80 0.12 930 0.04 0.01 0.25 0.10 96 99 T, <10% 80 0.12 930 0.04 0.01 0.01 0.16 0.04 99 99 T, <10% 80 0.12 930 0.04 0.01 0.01 0.16 0.04 99 99 T, <10% 80 0.12 930 0.04 0.01 0.01 0.16 0.04 99 99 T, <10% 80 0.12 930/97/24 0.12 0.10 0.40 0.38 88 90 T, <10% 80 0.12 939/97/2 0.12 0.10 0.40 0.38 88 90 T, <10% 80 0.15 939/97/2 0.12 0.10 0.40 0.38 88 90 T, <10% 80 0.15 937/84 0.08 0.06 0.33 0.30 0.92 94 T, <10% 80 0.15 937/84 0.08 0.06 0.33 0.30 0.92 94 T, <10% 80 0.15 937/84 0.08 0.06 0.33 0.30 0.99 97 T, <10% 80 0.15 937/84 0.08 0.06 0.33 0.30 0.99 99 T, <10% 80 0.15 938/284 0.15 0.12 0.45 0.48 84 86 > 10%, T, <20% 40 0.15 937/84 0.08 0.06 0.33 0.30 0.99 99 T, <10% 80 0.15 938/284 0.15 0.12 0.45 0.48 84 86 > 10%, T, <20% 40 0.15 939/97/97 0.16 0.14 0.14 0.46 0.45 84 86 > 10%, T, <20% 40 0.15 939/97/97 0.16 0.14 0.40 0.39 9.38 9.39 7, <10% 80 0.15 939/97/97 0.16 0.14 0.14 0.46 0.45 84 86 9 > 10%, T, <20% 40 0.15 939/97/97 0.16 0.18 0.09 0.33 0.33 90 99 T, <10% 80 0.15 938/98/97 0.19 0.19 0.18 0.55 0.50 88 91 T, <10% 80 0.15 938/99/97 0.19 0	URBAN STYLE									
981/929	980/2	0.19	0.18	0.54	0.53	81	82	>10%, T _v <20%	40	0.18
975/926 0.19 0.16 0.52 0.49 81 84 >10%, T, <20% 40 0.15 976/926 0.11 0.09 0.42 0.39 89 91 T, <10% 80 0.14 969 0.19 0.17 0.53 0.50 81 83 >10%, T, <20% 40 0.15 983/926 0.09 0.07 0.38 0.35 91 93 T, <10% 80 0.13 983/926 0.09 0.07 0.38 0.35 91 93 T, <10% 80 0.13 982/97 0.13 0.10 0.43 0.39 88 92 T, <10% 80 0.13 407/14 0.12 0.08 0.41 0.37 88 92 T, <10% 80 0.15 982/97 0.13 0.10 0.43 0.39 88 92 T, <10% 80 0.15 985/15 0.17 0.13 0.43 0.40 83 87 >10%, T, <20% 40 0.15 985/15 0.17 0.13 0.43 0.40 83 87 >10%, T, <20% 40 0.15 986 0.07 0.04 0.39 0.34 93 96 T, <10% 80 0.13 929 0.20 0.18 0.55 0.53 80 82 >10%, T, <20% 40 0.15 930 0.04 0.01 0.25 0.10 96 99 T, <10% 80 0.15 930 0.04 0.01 0.25 0.10 96 99 T, <10% 80 0.15 930 0.04 0.01 0.25 0.10 96 99 T, <10% 80 0.15 976/84 0.17 0.14 0.52 0.48 83 86 >10%, T, <20% 40 0.16 976/84 0.17 0.14 0.52 0.48 83 86 >10%, T, <20% 40 0.16 976/84 0.15 0.12 0.46 0.49 85 88 >10%, T, <20% 40 0.16 976/84 0.15 0.12 0.45 0.40 85 88 >10%, T, <20% 40 0.16 976/84 0.15 0.12 0.45 0.40 85 88 >10%, T, <20% 40 0.16 978/79 0.16 0.14 0.46 0.45 84 86 >10%, T, <20% 40 0.16 978/79 0.16 0.14 0.46 0.45 84 86 >10%, T, <20% 40 0.16 978/79 0.16 0.14 0.46 0.45 84 86 >10%, T, <20% 40 0.16 978/79 0.16 0.14 0.46 0.45 84 86 >10%, T, <20% 40 0.16 978/79 0.16 0.14 0.46 0.45 84 86 >10%, T, <20% 40 0.16 978/79 0.16 0.14 0.46 0.45 84 86 >10%, T, <20% 40 0.16 978/79 0.16 0.14 0.46 0.45 84 86 >10%, T, <20% 40 0.16 978/79 0.16 0.14 0.46 0.45 84 86 >10%, T, <20% 40 0.16 978/79 0.16 0.14 0.46 0.45 84 86 >10%, T, <20% 40 0.16 979/79 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	979/1	0.10	0.08	0.35	0.34	90	92	T _v <10%	80	0.14
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977/926 0.11 0.09 0.42 0.39 89 91 T _V <10% 80 0.12 983/926 0.09 0.17 0.53 0.50 81 83 >10%, T _V <20% 40 0.15 983/926 0.09 0.07 0.38 0.35 91 93 T _V <10% 80 0.13 982/97 0.13 0.10 0.43 0.39 87 90 >10%, T _V <20% 80 0.13 407/14 0.12 0.08 0.41 0.37 88 92 T _V <10% 80 0.15 407/926 0.18 0.17 0.52 0.49 82 83 >10%, T _V <20% 40 0.15 996/60 0.07 0.04 0.39 0.34 93 96 T _V <10% 80 0.11 926 0.07 0.04 0.39 0.34 93 96 T _V <10% 80 0.11 929 0.20 0.18 0.55 0.53 80 82 >10%, T _V <20% 40 0.11 930 0.04 0.01 0.25 0.10 96 99 T _V <10% 80 0.12 930 0.04 0.01 0.25 0.10 96 99 T _V <10% 80 0.16 937/97/2 0.12 0.10 0.40 0.38 88 90 T _V <10% 80 0.16 997/9/2 0.12 0.10 0.40 0.38 88 90 T _V <10% 80 0.19 991/84 0.08 0.66 0.33 0.30 92 94 T _V <10% 80 0.16 997/84 0.15 0.12 0.45 0.40 85 88 10%, T _V <20% 40 0.16 997/84 0.15 0.15 0.12 0.45 0.40 85 88 10%, T _V <20% 40 0.16 997/84 0.17 0.14 0.52 0.48 83 86 >10%, T _V <20% 40 0.16 997/84 0.17 0.14 0.52 0.48 83 86 >10%, T _V <20% 40 0.16 997/84 0.17 0.14 0.52 0.48 83 86 >10%, T _V <20% 40 0.16 997/84 0.10 0.08 0.66 0.33 0.30 92 94 T _V <10% 80 0.16 998/87 0.16 0.14 0.46 0.45 84 83 86 >10%, T _V <20% 40 0.16 998/87 0.16 0.14 0.46 0.45 84 86 >10%, T _V <20% 40 0.16 998/87 0.16 0.14 0.46 0.45 84 86 >10%, T _V <20% 40 0.16 998/87 0.16 0.14 0.46 0.45 84 86 >10%, T _V <20% 40 0.16 998/87 0.16 0.14 0.46 0.45 84 86 >10%, T _V <20% 40 0.16 998/87 0.16 0.14 0.46 0.45 84 86 >10%, T _V <20% 40 0.16 998/87 0.16 0.14 0.46 0.45 84 86 >10%, T _V <20% 40 0.16 998/87 0.16 0.14 0.46 0.45 84 86 >10%, T _V <20% 40 0.16 998/87 0.16 0.14 0.46 0.45 84 86 >10%, T _V <20% 40 0.16 998/97 0.10 0.10 0.08 0.37 0.32 90 92 T _V <10% 80 0.16 999 0.20 0.18 0.55 0.53 80 82 >10%, T _V <20% 40 0.16 998/98 0.00 0.00 0.00 0.33 0.30 92 94 T _V <10% 80 0.16 999 0.20 0.18 0.55 0.50 0.50 83 85 >10%, T _V <20% 40 0.16 999 0.20 0.18 0.55 0.50 0.50 83 85 >10%, T _V <20% 40 0.16 990 0.20 0.18 0.55 0.50 0.50 83 85 >10%, T _V <20% 40 0.16 990 0.20 0.18 0.55 0.50 0.50 83 85 >10%, T _V <20% 40 0.16 990 0.10 0.00 0.00 0.00 0.00 0.00 0.00 0	975/926	0.19	0.16	0.52	0.49	81	84	>10%, T _v <20%	40	0.19
983/926	977/926	0.11	0.09	0.42	0.39	89	91		80	0.14
982,97 0.13 0.10 0.43 0.39 87 90 \$10\%, T_v < 20\% 80 0.15 407/14 0.12 0.08 0.41 0.37 88 92 \$1_v < 10\% T_v < 20\% 80 0.15 407/14 0.12 0.08 0.41 0.37 88 92 \$1_v < 10\%, T_v < 20\% 40 0.18 68/15 0.17 0.13 0.43 0.40 83 87 \$10\%, T_v < 20\% 40 0.18 68/15 0.17 0.13 0.43 0.40 83 87 \$10\%, T_v < 20\% 40 0.18 926 0.07 0.04 0.39 0.34 93 96 T_v < 10\%, T_v < 20\% 40 0.15 929 0.20 0.18 0.55 0.53 80 82 \$10\%, T_v < 20\% 40 0.15 930 0.04 0.01 0.25 0.10 96 99 T_v < 10\% 80 0.11 930 0.04 0.01 0.05 0.04 99 99 T_v < 10\% 80 0.12 944 0.01 0.01 0.16 0.04 99 99 T_v < 10\% 80 0.12 944 0.01 0.10 0.16 0.04 99 99 T_v < 10\% 80 0.12 981/84 0.08 0.06 0.33 0.30 92 94 T_v < 10\% 80 0.12 991/584 0.15 0.12 0.45 0.40 85 88 \$10\%, T_v < 20\% 40 0.16 997/84 0.15 0.12 0.45 0.40 85 88 \$10\%, T_v < 20\% 40 0.16 997/84 0.08 0.06 0.34 0.26 92 94 T_v < 10\% 80 0.12 997/84 0.08 0.06 0.34 0.26 92 94 T_v < 10\% 70\% 80 0.12 997/84 0.08 0.06 0.34 0.26 92 94 T_v < 10\% 70\% 80 0.12 9982/84 0.10 0.08 0.37 0.32 90 92 T_v < 10\% 80 0.12 907/84 0.16 0.14 0.46 0.45 84 86 \$10\%, T_v < 20\% 40 0.16 907/84 0.16 0.14 0.46 0.45 84 86 \$10\%, T_v < 20\% 40 0.16 907/84 0.16 0.14 0.46 0.45 84 86 \$10\%, T_v < 20\% 40 0.16 907/84 0.10 0.10 0.08 0.37 0.32 90 92 T_v < 10\% 80 0.12 907/84 0.10 0.10 0.80 0.37 0.32 90 92 T_v < 10\% 80 0.12 907/84 0.16 0.14 0.46 0.45 84 86 \$10\%, T_v < 20\% 40 0.16 907/84 0.16 0.14 0.11 0.45 0.42 86 89 \$10\%, T_v < 20\% 40 0.16 907/84 0.16 0.13 0.51 0.46 84 87 \$10\%, T_v < 20\% 40 0.16 907/84 0.16 0.13 0.51 0.46 84 87 \$10\%, T_v < 20\% 40 0.15 908/84 0.05 0.01 0.23 0.10 95 99 T_v < 10\% 80 0.11 909/909 0.00 0.00 0.00 0.00 0.00 0.00 0.	969	0.19	0.17	0.53	0.50	81	83	>10%, T _v <20%	40	0.19
	983/926	0.09	0.07	0.38	0.35	91	93	T _v <10%	80	0.13
407/926	982/97	0.13	0.10	0.43	0.39	87	90	>10%, T _v <20%	80	0.15
58/15	407/14	0.12	0.08	0.41	0.37	88			80	0.15
926	407/926	0.18	0.17	0.52	0.49	82		>10%, T _v <20%	40	0.18
929	58/15	0.17	0.13	0.43	0.40			$>10\%$, $T_{v} < 20\%$	40	0.18
14	926	0.07	0.04	0.39	0.34	93	96	T _v <10%	80	0.11
930	929	0.20	0.18	0.55	0.53	80		>10%, T _v <20%	40	0.19
COUNTRY STYLE 980/3 0.19 0.18 0.55 0.54 81 82 10%, T _v < 20% 40 0.18 997/2 0.12 0.10 0.40 0.38 88 90 T _v < 10%, T _v < 20% 40 0.18 997/8/4 0.08 0.06 0.33 0.30 92 94 T _v < 10% 80 0.12 996/84 0.17 0.14 0.52 0.48 83 86 10%, T _v < 20% 40 0.16 997/84 0.08 0.06 0.34 0.26 92 94 T _v < 10% 80 0.12 9978/7 0.16 0.14 0.16 0.14 0.10 0.45 0.40 85 88 10%, T _v < 20% 40 0.17 998/84 0.10 0.08 0.06 0.34 0.26 92 94 T _v < 10% 80 0.12 997/84 0.00 0.01 0.08 0.37 0.32 90 92 T _v < 10% 80 0.12 998/97/76 0.16 0.14 0.11 0.45 0.42 86 89 10%, T _v < 20% 40 0.17 998/76 0.10 0.08 0.37 0.32 90 92 T _v < 10% 80 0.12 407/16 0.14 0.11 0.45 0.42 86 89 10%, T _v < 20% 40 0.17 998/98 0.10 80 0.11 90 90 90 90 10, 10% 80 0.11 90 90 90 10, 10% 80 0.11 90 90 90 10, 10% 80 0.11 90 90 90 10, 10% 80 0.11 90 90 90 10, 10% 80 0.11 90 90 90 10, 10% 80 0.11 90 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 80 0.11 90 90 10, 10% 90 90 10, 10% 90 10, 10% 90 90 10, 1	14	0.07	0.02	0.34	0.27		98	T _v <10%	80	0.12
COUNTRY STYLE 980/3	930	0.04	0.01	0.25	0.10	96	99	T _v <10%	80	0.10
980/3	24	0.01	0.01	0.16	0.04	99	99	$T_{v} < 10\%$	80	0.09
979/2	COUNTRY STYLE									
979/2 0.12 0.10 0.40 0.38 88 90 T _v <10% 80 0.15 981/84 0.08 0.06 0.33 0.30 92 94 T _v <10% 80 0.12 995/844 0.17 0.14 0.52 0.48 83 86 >10%, T _v <20% 40 0.17 975/84 0.15 0.12 0.45 0.40 85 88 >10%, T _v <20% 40 0.16 977/84 0.08 0.06 0.34 0.26 92 94 T _v <10% 80 0.12 978/7 0.16 0.14 0.46 0.45 84 86 >10%, T _v <20% 40 0.17 982/84 0.10 0.08 0.37 0.32 90 92 T _v <10% 80 0.12 407/16 0.14 0.11 0.45 0.42 86 89 >10%, T _v <20% 80 0.12 407/84 0.16 0.13 0.51 0.46 84 87 >10%, T _v <20% 80 0.13 407/84 0.16 0.13 0.51 0.46 84 87 >10%, T _v <20% 80 0.13 84 0.05 0.01 0.23 0.10 95 99 T _v <10% 80 0.11 929 0.20 0.18 0.55 0.53 80 82 >10%, T _v <20% 40 0.17 930 0.04 0.01 0.25 0.10 96 99 T _v <10% 80 0.11 51/1 0.17 0.15 0.50 0.50 83 85 >10%, T _v <20% 40 0.17 930 0.04 0.01 0.25 0.10 96 99 T _v <10% 80 0.11 856 SIDE 856 SIDE 857 0.09 0.07 0.04 0.31 0.40 88 91 T _v <10% 80 0.16 938/14 0.12 0.09 0.43 0.40 88 91 T _v <10% 80 0.16 938/14 0.12 0.09 0.43 0.40 88 91 T _v <10% 80 0.16 938/14 0.12 0.09 0.43 0.40 88 91 T _v <10% 80 0.16 938/14 0.12 0.09 0.41 0.39 88 91 T _v <10% 80 0.16 938/14 0.12 0.09 0.43 0.40 88 91 T _v <10% 80 0.16 938/14 0.12 0.09 0.43 0.40 88 91 T _v <10% 80 0.16 938/14 0.12 0.09 0.43 0.40 88 91 T _v <10% 80 0.16 938/14 0.12 0.09 0.41 0.39 88 91 T _v <10% 80 0.16 938/14 0.12 0.09 0.41 0.39 88 91 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.10 0.06 0.33 0.30 90 94 T _v <10% 80 0.16 938/14 0.10 0.10 0.10 0.10 0.10	980/3	0.19	0.18	0.55	0.54	81	82	>10%, T _v <20%	40	0.18
981/84	979/2	0.12	0.10	0.40	0.38	88	90	T _v <10%	80	0.15
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	981/84	0.08	0.06	0.33	0.30	92	94		80	0.12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	976/84	0.17	0.14	0.52	0.48	83	86		40	0.17
977/84	975/84	0.15	0.12	0.45	0.40	85	88		40	0.16
978/7 0.16 0.14 0.14 0.46 0.45 84 86 510%, T _V < 20% 40 0.17 982/84 0.10 0.08 0.37 0.32 90 92 T _V < 10% 80 0.13 407/16 0.14 0.11 0.45 0.42 86 89 510%, T _V < 20% 80 0.16 0.16 0.17 7 0.04 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.03 0.01 0.03 0.01 0.04 0.01 0.05 0.01 0.05 0.01 0.07 0.04 0.01 0.05 0.01 0.07 0.04 0.01 0.05 0.07 0.04 0.01 0.05 0.07 0.04 0.01 0.05 0.07 0.04 0.01 0.05 0.00 0.07 0.04 0.01 0.05 0.00 0.01 0.01 0.01 0.02 0.00 0.01 0.01 0.01 0.02 0.01 0.02 0.02 0.03 0.04 0.01 0.05	977/84	0.08	0.06	0.34	0.26	92	94		80	0.12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	978/7	0.16	0.14	0.46	0.45	84	86	>10%, T _v <20%	40	0.17
Math	982/84	0.10	0.08	0.37	0.32	90	92		80	0.13
0.04	407/16	0.14	0.11	0.45	0.42	86	89		80	0.16
84	407/84	0.16	0.13	0.51					40	0.17
929	7	0.04	0.01					$T_{v} < 10\%$		0.11
926	84	0.05	0.01	0.23	0.10			$T_{v} < 10\%$		0.11
15/1	929	0.20	0.18	0.55	0.53	80	82		40	0.19
SEA SIDE 0.04 0.01 0.25 0.10 96 99 T _v <10% 80 0.10 980/1 0.11 0.07 0.39 0.36 89 93 T _v <10%	926	0.07	0.04				96		80	0.11
SEA SIDE 980/1 0.11 0.07 0.39 0.36 89 93 T _V <10%	15/1							>10%, T _v <20%		0.17
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	930	0.04	0.01	0.25	0.10	96	99	T_{v} <10%	80	0.10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	SEA SIDE									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	980/1	0.11	0.07	0.39	0.36	89	93	T _v <10%	80	0.14
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	979/3	0.12	0.09	0.43	0.40	88	91		80	0.14
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	974/87	0.14	0.11	0.48	0.45	86	89		80	0.15
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	985/87	0.09	0.07	0.33	0.31	91	93		80	0.13
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	981/14	0.12	0.09	0.41	0.39	88	91		80	0.15
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	984/14	0.10	0.06	0.33	0.30	90	94		80	0.14
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	978/92	0.14	0.12	0.44	0.42	86	88		80	0.16
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	983/92	0.08	0.04	0.28	0.20	92	96		80	0.13
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	782/14	0.19	0.15		0.51	85	89			0.18
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	782/87	0.14	0.11	0.49	0.43	86	89	>10%, T _v <20%	80	0.15
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	14	0.07	0.02	0.34		93	98		80	0.12
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	87	0.04	0.01	0.21	0.05	96	99		80	0.11
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15	0.27	0.26	0.67	0.67	73	74		30	0.23
	15/1	0.17	0.15	0.50	0.50	83	85		40	0.17
92 0.01 0.01 0.15 0.05 99 99 T <10% 80 0.00	98	0.05	0.01	0.21	0.09	95	99		80	0.11
<u>52</u>	92	0.01	0.01	0.15	0.05	99	99	T _v <10%	80	0.09



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